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(54) **A receiver-transmitter for a target identification system.**

(57) A receiver-transmitter for a target identification system having a particular but not necessarily an exclusive application for the identification of aircraft which utilises laser vibrometry and a coherent array receiver including an array of photodetectors adapted to receive signals from different parts of the target and to use a corresponding array of frequency-offset reference beams to provide coherent detection of each of the received signals.

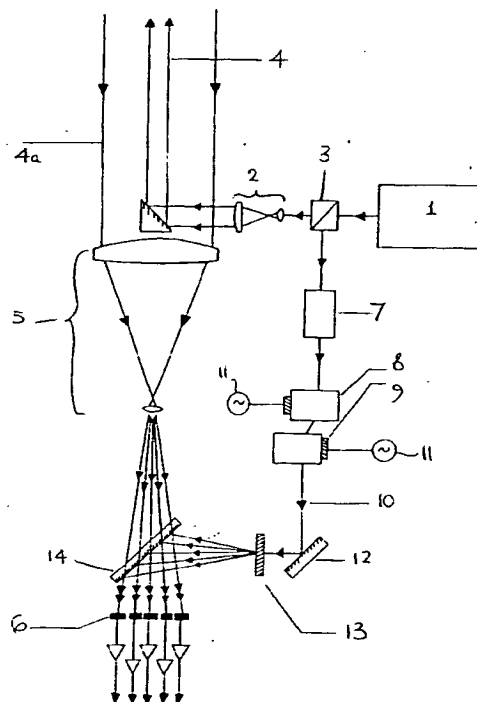


FIGURE 1

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The invention relates to a receiver-transmitter for a target identification system having a particular but not necessarily an exclusive application for the identification of aircraft.

The identification of targets such as aircraft utilising lasers involves the coherent detection of scattered light from the targets which in the case of aircraft, would be travelling at high speed and would, therefore, produce a large Doppler-shift in the received signal. For a laser wavelength of 1 μm , the Doppler shift is 2 MHz per meter/second of relative target velocity. Thus, for aircraft travelling towards an observer at Mach 2, the Doppler shift is of the order of 1 GHz. A laser vibrometer detection system would have to lock onto this Doppler frequency and measure the frequency modulation imposed by the target vibration.

With such an arrangement, the FM sidebands would be only a few kHz away from the centre frequency and so could be difficult to detect, especially if the signal-to-noise ratio of the return signal from the target is low.

A major problem with such systems is laser frequency stability which introduces FM noise into the coherently detected signal, and so affects the ability of the system to detect signal sidebands close-in to the carrier. This is a serious problem at long range, where the long time delay between transmitted and return signals introduces a large amount of phase-decorrelation between signal and reference beams in the receiver, leading to enhanced FM noise.

The identification of targets utilising lasers and, in particular, laser vibrometry is normally effected by focusing a laser beam onto a diffraction-limited spot on the surface of the target and by detecting the backscatter from the target by means of a telescope located adjacent to or coaxial with the laser transmitter. The light wave received at the telescope is focused onto a photodetector where it is combined with a low-power reference wave derived from the laser transmitter. Interference between the two waves generates a heterodyne photocurrent on the photodetector which is selected by a phase-locked loop tracking filter. Periodic variations in the Doppler frequency due to target vibration appear as a modulation voltage in the phase-locked loop output.

A system for detecting vibration signatures from targets such as aircraft will require either some means for locking the transmitted beam onto the relevant part of the aircraft surface whilst the vibration signature is being detected, or a relatively wide-field transmitted beam which illuminates a substantial area and does not require precise beam positioning on the target.

In view of the difficulty of locking beams onto high speed targets such as aircraft, some form of array receiver is required for detecting/identifying such targets.

It is an object of the present invention to overcome the difficulties, referred to above, of locking beams onto high speed targets by providing a receiver-transmitter for target identification systems which utilises laser vibrometry and a coherent array receiver.

The invention provides a receiver-transmitter for a target identification system including laser means for generating and focusing a laser beam onto the reflective surface of a target to be identified, collection means for collecting the reflected signal from the target, an array of photodetectors onto at least one of which the collected signals is focused, generation means connected to the output of the laser means for generating a frequency-shifted reference beam from the laser beam, beam division means for dividing the reference beam into a number of separate reference beams, each having substantially equal power, and beam splitting means for causing each of the reference beams to be focused onto a separate one of the photodetectors of the array, the focusing of the collected signal onto the photodetector array being such that the reference and collected beams incident on the same photodetector are collinear.

According to one aspect of the present invention a receiver-transmitter for a target identification system is provided which includes, for each of the photodetectors of the array, amplifying means connected to the photodetector output and frequency demodulation means connected to the output of the amplifying means.

According to another aspect of the present invention a receiver-transmitter for a target identification system is provided which includes beam steering means for directing the laser beam in the direction of the target.

The photodetector array can be in the form of an $N \times N$ rectangular array or a quadrant array of four photodetectors.

The beam division means can be either a Dammann grating or a hologram which provide a means of effecting coherent detection of each signal.

The utilisation of a receiver-transmitter according to the present invention in a target identification system may also require the use of at least one retroreflective device located on or in the surface of the target, for example an aircraft, to be detected in order to increase the signal-to-noise ratio of the return signal from the target and to thereby extend the range of the identification system. Such retroreflective devices could be provided by the retroreflective devices covered by our co-pending patent applications P/8886/ARO and P/8873/ARO.

The foregoing and other features according to the present invention will be better understood from the following description with reference to the accompanying drawings, in which:-

Figure 1 illustrates in the form of a block diagram

a receiver-transmitter according to the present invention for a target identification system, Figure 2 illustrates in a plan view part of one arrangement for a photodetector array for the receiver-transmitter illustrated in Figure 1, Figure 3 illustrates in a plan view another arrangement for a photodetector array for the receiver-transmitter illustrated in Figure 1, Figure 4 illustrates in the form of a block diagram a frequency demodulation circuit for the receiver-transmitter illustrated in Figure 1, and Figure 5 illustrates a target identification system which includes the receiver-transmitter illustrated in Figure 1.

A receiver-transmitter according to the present invention for a target identification system is illustrated in Figure 1 of the drawings and includes a single frequency CW Neodymium-YAG laser 1 the laser beam output of which is connected to a telescope 2 via a beam splitter 3. The laser beam is expanded by the telescope 2 to form a slightly diverging beam 4 which is focused onto a remote target to be identified by a scanning mirror system (not shown in Figure 1).

The target onto which the laser beam is focused may, for example, be an aircraft, and the light 4a scattered by the surface of the aircraft and/or a retro-reflective device located in or on the surface of the aircraft is returned in the direction of the receiver-transmitter and is collected by a receiving telescope 5 after passing in the reverse direction through the scanning mirror system referred to above.

In order to minimise the overall aperture of the scanning mirror system, it is convenient to make the transmitted and collected beams 4 and 4a respectively coaxial as illustrated in Figure 1.

The receiver-transmitter of Figure 1 also includes an array 6 of photodetectors onto at least one of which the reflected beam 4a is focused by the telescope 5. The array 6 of photodetectors could for example be in the form of a rectangular array of $N \times N$ photodetectors 25 as shown in Figure 2 of the drawings. Alternatively, the array 6 of photodetectors could be a quadrant array of 4 photodetectors 26 as illustrated in Figure 3 of the drawings.

In operation, if the angular position of the target changes, while it remains within the limited angular field of the transmitted laser beam, then the return beam 4a will be caused to move from one photodetector in the array 6 to another one of the photodetectors in the array 6.

The beam splitter 3 causes part of the laser beam output of the laser 1 to be diverted to an optical isolator 7 the output of which is connected to the input of a pair of cascaded acousto-optic frequency shifters 8 and 9. The output of the frequency shifters 8 and 9 provides a reference beam 10 for the receiver-transmitter. The cascaded frequency shifters 8 and 9 are identical devices driven from the same R.F. frequency

generators 11 so that the light output of the isolator 7 which is diffracted through both of the frequency shifters 8 and 9, emerges undeflected at the output of frequency shifters 8 and 9, but shifted in frequency by twice the frequency of the generators 11. This arrangement provides a convenient means for changing the frequency of the laser beam output of the laser by a known amount without causing a change in beam direction.

The frequency-shifted reference beam 10 is deflected by a mirror 12 and passes through a beam divider 13 which divides the reference beam 10 into a number of separate beams each having substantially equal power and relatively small angular displacements relative to each other.

The array of reference beams emerging from the beam divider 13 is directed by a beam splitter 14 in such a direction that each reference beam is focused onto a separate one of the photodetectors of the array 6. The optical geometry of the beam splitter 14 is such that the reference and collected beams incident on the same photodetector are collinear. The beam divider 13 can, for example, be a Dammann grating or a hologram which provides a means of effecting detection of each signal.

Interference between the reference and collected beams on the surface of a photodetector produces an AC photocurrent in the photodetector output at a frequency equal to the difference between the reference and collected beam frequencies. This process is normally referred to as heterodyne mixing.

The heterodyne frequency is equal to the total frequency shift in the reference beam introduced by the acousto-optic frequency shifters 8 and 9, minus the Doppler frequency shift in the collected beam produced by relative motion between the remote target that is being detected and the receiver-transmitter. The R.F. frequency applied to the frequency shifters 8 and 9 can be adjusted in accordance with the relative velocity of the target, to substantially cancel out the Doppler shift arising from target motion, to produce a heterodyne current in the photodetector output at a conveniently low frequency. This could, for example, be 1 MHz which is easy to process by conventional low-speed circuits.

The heterodyne photocurrent from each photodetector in the array is separately processed by a number of identical circuits as illustrated in Figure 4 of the drawings. As illustrated in Figure 4, the photocurrent output of each of the photodetectors of the array 6 is amplified by an amplifier 15 and is passed to a frequency demodulator 16 which produces an output proportional to small deviations in input frequency about the mean frequency. The frequency demodulators 16 could be provided by any one of a number of conventional demodulators used in FM radio receivers.

The output of each of the demodulators 16 is pro-

portional to small changes in target velocity, and therefore provides an analogue of the oscillatory motion of the target created by applied vibration.

With vibrating targets such as an aircraft, some means is required for controlling the direction of the transmitted laser beam to ensure that it continually illuminates the target while it is rapidly moving. This can be achieved by measuring the relative amplitudes of the heterodyne signals utilising the photodetector array illustrated in Figure 3 of the drawings.

If it is assumed that the target is initially aligned on the centre of the photodetector array, then the outputs from all four photodetectors 26 of the array will be the same. Small movements in target position will deflect the collected beam 4a thereby causing an imbalance in signals from each of the photodetectors 26 of the array. Measurement of the relative amplitudes of the heterodyne signals from each photodetector 26 will therefore indicate the magnitude and direction of target motion. Correction signals can therefore be derived from differences in relative amplitude between one photodetector and another photodetector and the drive mechanism for the beam steering mirror system located in front of the receiver-transmitter can be operated to effect realignment of the collected beam 4a onto the centre of the photodetector array. With this arrangement, the transmitted laser beam 4 can be utilised to track the motion of a target.

The output signal of the demodulator 16 of each of the photodetectors of the array 6 is dependent not only on target vibration, but also on laser frequency variations, and on random fluctuations in the refractive index of the atmospheric path between the receiver-transmitter and the target. The laser frequency normally varies in a random fashion, with a typical spectral width of a few kHz, which may be of sufficient magnitude to interfere with vibration signals from the target.

The spurious output signals from these sources may be largely removed by using the target identification system which is illustrated in Figure 5 of the drawings in the form of a block diagram.

As illustrated in Figure 5, the target identification system includes two retroreflective devices 17 and 18 located on or in the surface of the target to be identified and a receiver-transmitter 19 of the type illustrated in Figure 1 of the drawings.

The retroreflective devices 17 and 18 may be provided by the retroreflective devices covered by our co-pending applications P/8887/ARO and P/8873/ARO. Such devices will greatly enhance the range of the target identification system because the retroreflective devices will cause the signal-to-noise ratio of the return signal 4a to be increased.

The receiver-transmitter 19 is adapted to cause the reflected signals from each of the retroreflective devices 17 and 18 to be incident on a separate photodetector 20 and 21.

The outputs from each of the photodetectors 20 and 21 respectively pass through separate amplifier/demodulator circuits 22 and 23 and are then compared in a difference circuit 24 which subtracts one signal from the other. Spurious signals arising from the factors referred to above produce equal signals on the two output signals of the amplifier/demodulator circuits 22 and 23 which are removed in the subtraction process effected by the circuit 24. The remaining signal emerging from the difference circuit 24 is therefore the difference in vibration amplitudes of the two retroreflective devices 17 and 18.

If only one of the retroreflected devices 17 and 18 is allowed to vibrate, then the difference signal at the output of the circuit 24 will be proportional to the vibration amplitude of the vibrating retroreflective device. Alternatively if both retroreflective devices are caused to vibrate at the same frequency, but in anti-phase, then the difference signal at the output of the circuit 24 will be proportional to twice the vibration amplitude of the retroreflective devices.

The modulation of the collected beam 4a could also be effected by incorporating a variety of devices in the target identification systems, for example, optical switching devices which could be used to effect modulation of the collected beam ie the backscattered light from the target, in order to provide a means for communicating, covert or otherwise, between the detected aircraft and the ground receiver-transmitter, or between two aircraft.

The use of high gain retroreflective devices in aircraft identification systems will increase the aircraft's visibility to hostile laser radar and it is, therefore, necessary to utilise in such systems a means of minimising this visibility. One method of achieving this would be to use narrow band wavelength-selective filters in front of the scattering surface or by selectively operating the optical switch referred to above only in response to a coded signal on the transmitted beam 4.

The activation of the optical switch could be effected by means of a photodetector located in the aircraft in close proximity to the retroreflective device. If the optical switch is normally closed, then on receipt of a coded signal on the transmitted beam 4 by the photodetector, the optical switch would be caused to open and the modulated signal would be returned to the receiver of the identification system, thus identifying a friendly aircraft.

The visibility of the retroreflective devices to hostile laser radar could also be minimised by reducing the physical size of the devices to the point where the absolute minimum signal-to-noise ratio is obtained at maximum range.

In an alternative arrangement for a target identification system, a number of the retroreflective devices could be arranged on the target in any desired form, for example, in the form of an alpha-numeric character, to provide an additional means of identi-

cation when the signal received from each of these devices are imaged onto the photodetector array 6 of the receiver-transmitter.

Claims

1. A receiver-transmitter for a target identification system characterised in that it includes laser means (1) for generating and focusing a laser beam (4) onto the reflective surface of a target to be identified, collection means (5) for collecting the reflected signal (4a) from the target, an array (6) of photodetectors onto at least one of which the collected signal (4a) is focused, generation means (3, 7, 8, 9, 11) connected to the output of the laser means (1) for generating a frequency-shifted reference beam (10) from the laser beam, beam division means (13) for dividing the reference beam (10) into a number of separate reference beams each having substantially equal power, and beam splitting means (14) for causing each of the reference beams to be focused onto a separate one of the photodetectors of the array (6), the focusing of the collected signal onto the photodetector array (6) being such that the reference and collected beams incident on the same photodetector are collinear.
2. A receiver-transmitter for a target identification system as claimed in claim 1 characterised in that it includes, for each of the photodetectors of the array (6), amplifying means (5) connected to the photodetector output and frequency demodulation means (16) connected to the output of the amplifying means (15).
3. A receiver-transmitter for a target identification system as claimed in claim 1 or claim 2 characterised in that the photodetector array (6) is a rectangular array of $N \times N$ photodetectors (25).
4. A receiver-transmitter for a target identification system as claimed in claim 1 or claim 2 characterised in that the photodetector array (6) is a quadrant array of four photodetectors (26).
5. A receiver-transmitter for a target identification system as claimed in any one of the preceding claims characterised in that the transmitted laser beam (4) and the reflected beam (4a) are substantially coaxial.
6. A receiver-transmitter for a target identification system as claimed in any one of the preceding claims characterised in that the generation means include a beam splitter (3) for causing part of the laser beam generated by the laser means (1) to be diverted to an optical isolator (7), a pair of cascaded acousto-optic frequency shifters (8,9) the input of which is connected to the output of the optical isolator (7), frequency drive means (11) for the cascaded frequency shifters (8,9) for causing the frequency of the output signal (10) of the cascaded frequency shifters (8,9) to be shifted by twice the frequency of the drive means (11).
7. A receiver-transmitter for a target identification system as claimed in any one of the preceding claims characterised in that the beam division means (3) is either a Dammann grating or a hologram.
8. A receiver-transmitter for a target identification system as claimed in any one of the claims 4 to 7 characterised in that it includes beam steering means for directing the laser beam (4) in the direction of the target.
9. A receiver-transmitter for a target identification system as claimed in claim 8 characterised in that the beam steering means include means connected to the outputs of the photodetector array (6) for measuring the relative amplitudes of the output signals of each of the photodetectors of the array and thereby deriving an output signal indicative of the position at which the collected signal (4a) is incident on the array (6), the output signal being utilised to drive the optical beam steering system of the receiver-transmitter to effect realignment of the collected beam (4a) onto the centre of the photodetector array (6).
10. A target identification system characterised in that it includes a receiver-transmitter as claimed in any one of the preceding claims.
11. A target identification system as claimed in claim 10 characterised in that it includes at least one retroreflective device (17, 18) located on or in the surface of a target to be detected.
12. A target identification system as claimed in claim 11 characterised in that it includes two retroreflective devices (17, 18) located on or in the surface of the target, a receiver-transmitter (19) as claimed in claim 2 adapted to cause the reflected signal from each of the retroreflective devices (17, 18) to be incident on a separate photodetector (20, 21) of the array, and means (24) for comparing the output signals of the demodulation means (22, 23) and providing a differential signal indicative of the difference in vibration amplitudes of the retroreflective devices (17, 18).

13. A target identification system as claimed in claim 12 characterised in that only one of the retroreflective devices (17, 18) is caused to vibrate and in that the difference signal is proportional to the vibration amplitude of the other one of the retroreflective devices (17, 18). 5
14. A target identification system as claimed in claim 12 characterised in that both retroreflective devices (17, 18) are caused to vibrate at the same frequency, but in antiphase, and in that the difference signal is proportional to twice the vibration amplitude of the retroreflective devices (17, 18). 10
15. A target identification system as claimed in claim 11 characterised in that it includes a geometrically distributed array (6) of retroreflective devices. 15
16. A target identification system as claimed in claim 15 characterised in that the array (6) of retroreflective devices are in the form of an alpha-numeric character. 20
17. A target identification system as claimed in any one of the claims 11 to 16 characterised in that it includes an optical switch for effecting modulation and/or selective blocking of the reflected signal (4a) from the said at least one retroreflective device (17, 18). 25
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18. A target identification system as claimed in any one of the preceding claims 11 to 17 characterised in that it includes narrow band wavelength-selective filters for filtering the reflected signal (4a) from the said at least one retroreflective device (17, 18). 35

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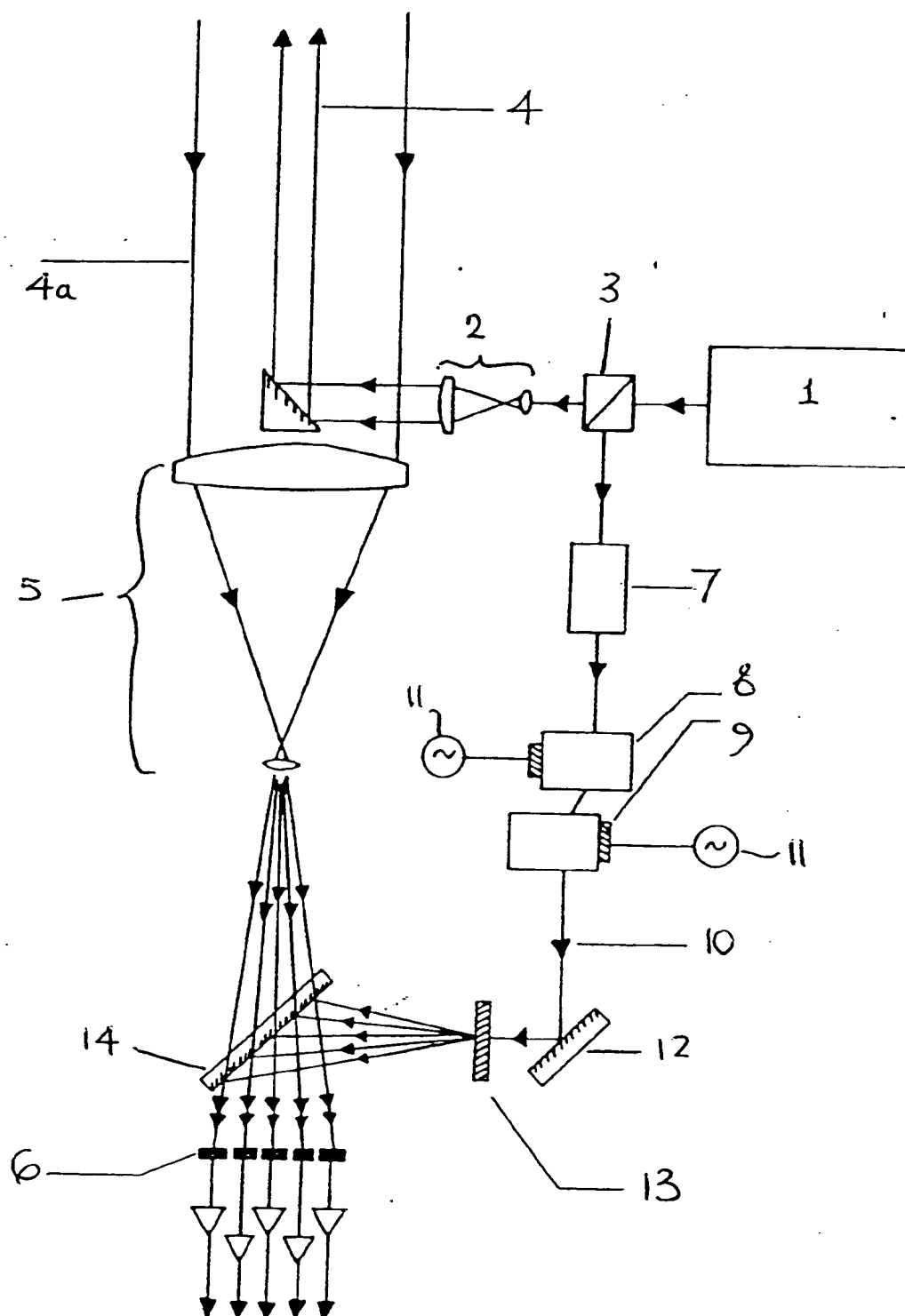


FIGURE 1

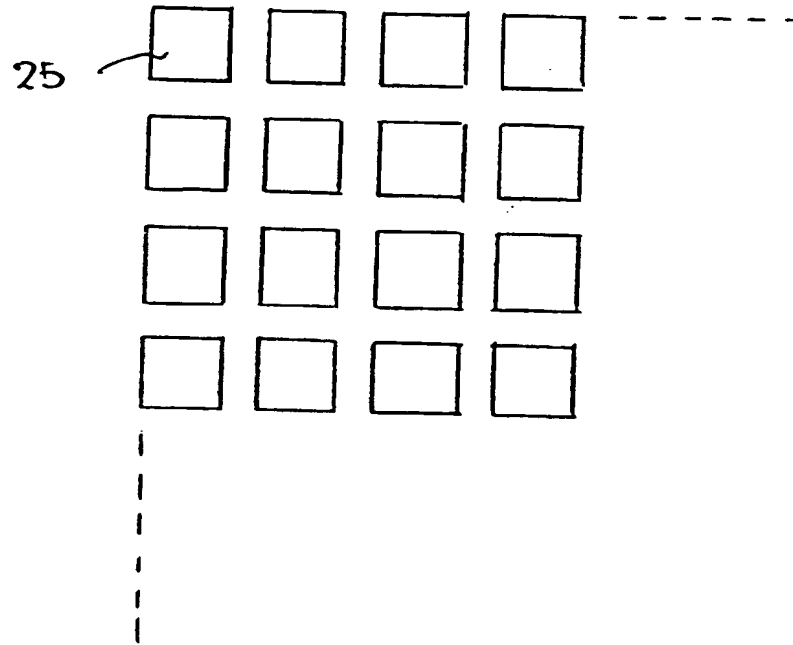


FIGURE 2

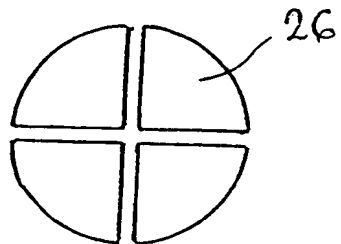


FIGURE 3

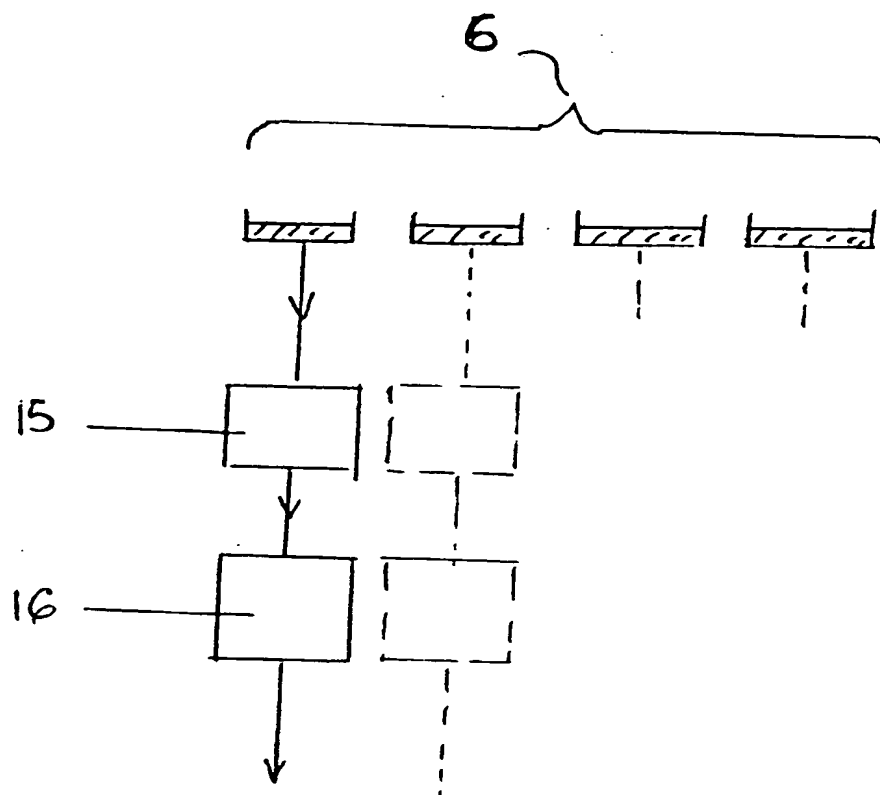


FIGURE 4

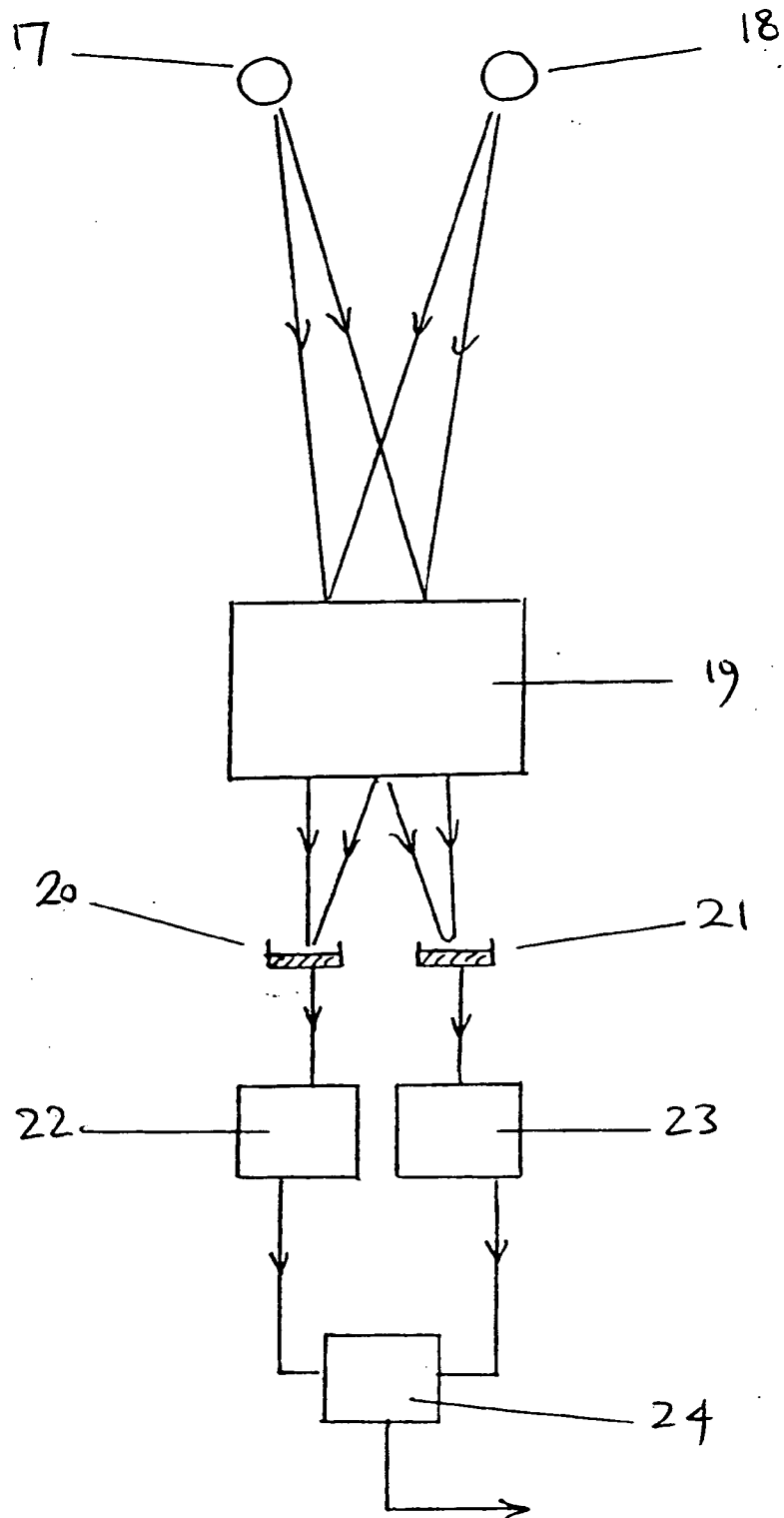


FIGURE 5



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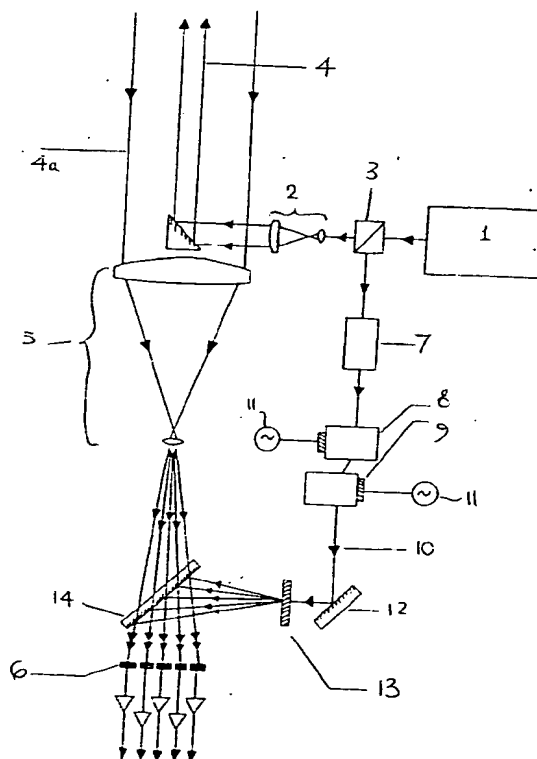


FIGURE 1

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EUROPEAN SEARCH REPORT

Application Number
EP 93 30 1865

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.5)
Y	GB-A-2 229 882 (SIEMENS) 3 October 1990 * abstract; figure 4 * * page 6, line 20 - page 8, line 4 * ---	1,5,7,10	G01S7/48 G01S17/88 G01S17/50 G01S17/74
Y	OPTICAL ENGINEERING. vol. 20, no. 6, November 1981, BELLINGHAM US pages 976 - 980 R.C. HARNEY 'Dual active/passive infrared imaging systems' * page 978, left column; figure 6 * ---	1,5,7,10	
A	---	6	
A	US-A-4 020 340 (COOKE) 26 April 1977 * abstract; figure 4 * ---	3,4,8,9	
A	US-A-4 887 310 (MEYZONNETTE ET AL.) 12 December 1989 * abstract; figure 1 * ---	1,10,11	
A	GB-A-2 145 894 (MESSERSCHMITT) 3 April 1985 * abstract * -----	17	
			TECHNICAL FIELDS SEARCHED (Int.Cl.5)
			G01S
The present search report has been drawn up for all claims			
Place of search THE HAGUE		Date of completion of the search 7 February 1994	Examiner Zaccà, F
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